## 2D and 3D FINITE ELEMENT METHOD

- Consider the following BVP in 2D (or 3D):

$$
\begin{align*}
-\nabla \cdot(\alpha \nabla u(\boldsymbol{r}))+\beta u(\boldsymbol{r}) & =f(\boldsymbol{r}), & & \boldsymbol{r} \in \Omega  \tag{82}\\
\left.u\right|_{\Gamma_{D}} & =g^{D}, & & \text { Dirichlet }  \tag{83}\\
\left.\alpha \frac{\partial u}{\partial n}\right|_{\Gamma_{N}} & =g^{N}, & & \text { Neumann } \tag{84}
\end{align*}
$$

- Here $u$ is a unknown function, $\alpha$ and $\beta$ are given coefficients, $f, g^{D}$ and $g^{N}$ are known functions, and $\Gamma=\Gamma_{D} \cup \Gamma_{N}, \Gamma_{D} \cap \Gamma_{N}=\emptyset$, is the boundary of $\Omega$.


## 2D and 3D FINITE ELEMENT METHOD

## Weak Formulation

- With Dirichlet boundary condition the weak formulation reads: Find $u \in H^{1}(\Omega), \gamma_{D} u=g^{D}$, so that

$$
\begin{equation*}
\langle\nabla w, \alpha \nabla u\rangle+\langle w, \beta u\rangle=\langle w, f\rangle \tag{85}
\end{equation*}
$$

holds for all $w \in H^{1}(\Omega), \gamma_{D} w=0$.

- With Neumann boundary condition the weak formulation reads: Find $u \in H^{1}(\Omega)$ so that

$$
\begin{equation*}
\langle\nabla w, \alpha \nabla u\rangle+\langle w, \beta u\rangle=-<w, g^{N}>_{\Gamma_{N}}+\langle w, f\rangle, \tag{86}
\end{equation*}
$$

holds for all $w \in H^{1}(\Omega)$.

## GENERAL RECIPE

## Weak Formulation

- Weak formulation can be obtained as follows. Multiply equation

$$
\begin{equation*}
-\nabla \cdot(\alpha \nabla u(\boldsymbol{r}))+\beta u(\boldsymbol{r})=f(\boldsymbol{r}), \tag{87}
\end{equation*}
$$

with a testing function $w \in H^{1}(\Omega)$ via the $L^{2}$ symmetric product

$$
\begin{equation*}
-\langle w, \nabla \cdot(\alpha \varepsilon(\boldsymbol{r}) \nabla u\rangle+\langle w, \beta \nabla u\rangle=\langle w, f\rangle . \tag{88}
\end{equation*}
$$

- Use identity

$$
\begin{equation*}
\nabla \cdot(u \boldsymbol{F})=\nabla u \cdot \boldsymbol{F}+u \nabla \cdot \boldsymbol{F}, \tag{89}
\end{equation*}
$$

with $\boldsymbol{F}=\alpha \nabla u$

$$
\begin{equation*}
-\langle w, \nabla \cdot(\alpha \nabla u)\rangle=\langle\nabla w, \alpha \nabla u\rangle+\int_{\Omega} \nabla \cdot(w \alpha \nabla u) d \Omega . \tag{90}
\end{equation*}
$$

- Then Gauss divergence theorem and boundary conditions give

$$
\begin{equation*}
\int_{\Omega} \nabla \cdot(w \alpha \nabla u) d \Omega=\langle w, \alpha \boldsymbol{n} \cdot \nabla u\rangle_{\Gamma_{N}}=\left\langle w, g^{N}\right\rangle_{\Gamma_{N}} . \tag{91}
\end{equation*}
$$

- Wanted weak formulation is obtained by combining above results.


## 2D and 3D FINITE ELEMENT METHOD

## Mesh and Finite Element Space

- A significant obvious difference compared to 1D is the mesh, i.e., geometrical element. In 2D we use triangles and in 3D tetras.


Figure: Triangle (2D) and tetra (3D) meshes.

- FE space $\left(T, P_{T}, \Sigma_{T}\right)$ consists of:
- Geometrical element $T$, a triangle (2D) or a tetra (3D).
- First order polynomial approximation on $T$.
- dof are the values of the approximation of $u$ at the nodes of $T$.


## 2D and 3D FINITE ELEMENT METHOD

## Basis Functions

- Use piece-wise linear continuous basis functions $u_{n}$

$$
\begin{equation*}
u(\boldsymbol{r}) \approx u^{h}(\boldsymbol{r})=\sum_{n=1}^{N_{N}} c_{n} u_{n}(\boldsymbol{r}) \tag{92}
\end{equation*}
$$

defined as ( $N_{n}$ and $N_{m}$ denote nodes of the mesh)

$$
u_{n}(\boldsymbol{r})=\left\{\begin{array}{cl}
1 & \text { if } \boldsymbol{r}=N_{n},  \tag{93}\\
0 & \text { if } \boldsymbol{r}=N_{m}, m \neq n, \\
\text { linear } & \text { otherwise } .
\end{array}\right.
$$



Figure: Support (left) and magnitude (right) of a linear nodal basis function.

## 2D and 3D FINITE ELEMENT METHOD

- This approximation is unisolvent and $H^{1}$ conforming.
- It defines a linear interpolation on each element.
- The total number of dof is the number of nodes of the mesh. (Note: Dirichlet boundary data fixes the values on the boundary).
- The number of elements (triangles) associated to a node depends on the mesh.
- Extension to 3D is straightforward.


## 2D and 3D FINITE ELEMENT METHOD

## Matrix Equation and Local Matrices

- Using Galerkin's method we obtain a matrix equation

$$
\begin{equation*}
\boldsymbol{A x}=\boldsymbol{b} \tag{94}
\end{equation*}
$$

with elements (without boundary conditions)

$$
\begin{align*}
A_{m n} & =\left\langle\nabla u_{m}, \alpha \nabla u_{n}\right\rangle+\left\langle u_{m}, \beta u_{n}\right\rangle  \tag{95}\\
b_{m} & =\left\langle u_{m}, f\right\rangle \tag{96}
\end{align*}
$$

- Similarly as in 1D, define local matrices and local vector

$$
\begin{align*}
& \operatorname{alok} 1(i, j)=\int_{T_{k}} N_{i}^{k}(\boldsymbol{r}) N_{j}^{k}(\boldsymbol{r}) d \boldsymbol{r},  \tag{97}\\
& \operatorname{alok} 2(i, j)=\int_{T_{k}} \nabla N_{i}^{k} \cdot \nabla N_{j}^{k} d \boldsymbol{r},  \tag{98}\\
& \operatorname{blok} 1(i)=\int_{T_{k}} N_{i}^{k}(\boldsymbol{r}) f(\boldsymbol{r}) d \boldsymbol{r},  \tag{99}\\
& i, j=1, \ldots, 3(2 \mathrm{D}), i, j=1, \ldots, 4 \text { (3D). Here } N_{i}^{k}=\left.u_{n}\right|_{T_{k}} .
\end{align*}
$$

## 2D and 3D FINITE ELEMENT METHOD

## System Matrix Assembly

for $k=1, \ldots$, number of elements do
\% Compute local matrices alok1 and alok2
for $i=1, \ldots, R+1$ do for $j=1, \ldots, R+1$ do
$\operatorname{alok} 1(i, j) \leftarrow \int_{T_{k}} N_{i}^{k}(\boldsymbol{r}) N_{j}^{k}(\boldsymbol{r}) d \boldsymbol{r}$
$\operatorname{alok} 2(i, j) \leftarrow \int_{T_{k}} \nabla N_{i}^{k}(\boldsymbol{r}) \cdot \nabla N_{j}^{k}(\boldsymbol{r}) d \boldsymbol{r}$
end for
end for
\% Add local matrices to the global one
for $i=1, \ldots, R+1$ do
for $j=1, \ldots, R+1$ do
$\boldsymbol{A}\left(n_{i}^{k}, n_{j}^{k}\right) \leftarrow \boldsymbol{A}\left(n_{i}^{k}, n_{j}^{k}\right)+\alpha_{k} \operatorname{alok} 2(i, j)+\beta_{k} \operatorname{alok} 1(i, j)$
end for
end for
end for

- Here $R=2$ (2D) or 3 (3D), $\alpha_{k}$ and $\beta_{k}$ are constants in $T_{k}$.


## 2D and 3D FINITE ELEMENT METHOD

## Source Vector Assembly

for $k=1, \ldots$, number of elements do
Compute local vector blok1
for $i=1, \ldots, R+1$ do
blok1 $(i) \leftarrow \int_{T_{k}} N_{i}^{k}(\boldsymbol{r}) f(\boldsymbol{r}) d \boldsymbol{r}$
end for
Add local vector to the global one
for $i=1, \ldots, R+1$ do
$\boldsymbol{b}\left(n_{i}^{k}\right) \leftarrow \boldsymbol{b}\left(n_{i}^{k}\right)+\operatorname{blok} 1(i)$
end for
end for

- Analogously to 1D, indeces $n_{i}^{k}$ and $n_{j}^{k}$ are given in 2D and 3D by

$$
\begin{equation*}
n_{i}^{k}=\operatorname{etopol}(i, k) \text { and } n_{j}^{k}=\operatorname{etopol}(j, k) . \tag{100}
\end{equation*}
$$

- The algorithms, and also how the boundary conditions are enforced are identical with the 1D case. What changes is the numerical evaluation of the matrix elements.


## 2D and 3D FINITE ELEMENT METHOD

- A 2D mesh can be described with nodes, edges and elements. Vertices of the elements (triangles) are called nodes.
- A triangular mesh can be defined using the following data structures

> coord : $\left(2 \times N_{N}\right)$ matrix; $x$ and $y$ coordinates of the nodes,
> etopol $:\left(3 \times N_{T}\right)$ matrix; indeces of the nodes of the elements.

- Here $N_{N}$ is the number of the nodes and $N_{T}$ is the number of the elements.
- The $x$ and $y$ coordinates of the vertices of an element $k$ are (Matlab notations):

$$
\begin{aligned}
& \text { p1 }=\operatorname{coord}(:, \operatorname{etopol}(1, k)) ; \\
& \text { p2 }=\operatorname{coord}(:, \operatorname{etopol}(2, k)) ; \\
& \text { p3 }=\operatorname{coord}(:, \operatorname{etopol}(3, k)) ;
\end{aligned}
$$

## 2D and 3D FINITE ELEMENT METHOD

- A tetra mesh in 3D can be defined using the following data structures

> coord $:\left(3 \times N_{N}\right)$ matrix; $x, y$ and $z$ coordinates of the nodes, etopol $:\left(4 \times N_{T}\right)$ matrix; indeces of the nodes of the elements.

- Here $N_{N}$ is the number of the nodes and $N_{T}$ is the number of the elements.
- The $x, y$ and $z$ coordinates of the vertices of an element $k$ are (Matlab notations):

$$
\begin{aligned}
& \text { p1 }=\operatorname{coord}(:, \operatorname{etopol}(1, k)) ; \\
& \text { p2 }=\operatorname{coord}(:, \operatorname{etopol}(2, k)) ; \\
& \text { p3 }=\operatorname{coord}(:, \operatorname{etopol}(3, k)) ; \\
& \text { p4 }=\operatorname{coord}(:, \operatorname{etopol}(4, k)) ;
\end{aligned}
$$

## 2D and 3D FINITE ELEMENT METHOD

## Evaluation of the Matrix Elements in 2D

- Let $\boldsymbol{p}_{j}^{k}, j=1,2,3$, denote the vertices of a triangle $T_{k}$.
- The vertices of a reference triangle $\hat{T}$ are $(0,0),(1,0)$ and $(0,1)$.
- Define a linear mapping $\mathcal{F}_{k}: \hat{T} \mapsto T_{k}$.
- Function $\mathcal{F}_{k}$ maps point $(0,0)$ to $\boldsymbol{p}_{1}^{k}$, point $(1,0)$ to $\boldsymbol{p}_{2}^{k}$ and point $(0,1)$ to $\boldsymbol{p}_{3}^{k}$.


Figure: Linear mapping $\mathcal{F}_{k}$ from a reference triangle $\hat{T}$ to a triangle $T_{k}$.

## 2D and 3D FINITE ELEMENT METHOD

## Evaluation of the Matrix Elements in 2D

- Mapping $\mathcal{F}_{k}$ can ${ }_{3}$ be defined as

$$
\begin{equation*}
\mathcal{F}_{k}(\xi, \eta):=\sum_{i=1}^{3} \boldsymbol{p}_{i}^{k} \hat{N}_{i}(\xi, \eta)=\left(\boldsymbol{p}_{2}^{k}-\boldsymbol{p}_{1}^{k}\right) \xi+\left(\boldsymbol{p}_{3}^{k}-\boldsymbol{p}_{1}^{k}\right) \eta+\boldsymbol{p}_{1}^{k}, \tag{101}
\end{equation*}
$$

where $\hat{N}_{i}, i=1,2,3$, are the nodal shape functions on $\hat{T}$

$$
\begin{align*}
& \hat{N}_{1}(\xi, \eta)=1-\xi-\eta,  \tag{102}\\
& \hat{N}_{2}(\xi, \eta)=\xi  \tag{103}\\
& \hat{N}_{3}(\xi, \eta)=\eta . \tag{104}
\end{align*}
$$



Fioıure: Linear nodal shane functions on a reference trianale.

## 2D and 3D FINITE ELEMENT METHOD

## Evaluation of the Matrix Elements in 2D

- Using mapping $\mathcal{F}_{k}$ we can write

$$
\begin{equation*}
\int_{T_{k}} u(x, y) d x d y=\int_{\hat{T}} u\left(\mathcal{F}_{k}(\xi, \eta)\right)\left|\operatorname{det}\left(J_{\mathcal{F}_{k}}\right)\right| d \xi d \eta \tag{105}
\end{equation*}
$$

where $J_{\mathcal{F}_{k}}$ is the Jacobian of $\mathcal{F}_{k}$, given as

$$
\begin{equation*}
J_{\mathcal{F}_{k}}=\left[\frac{\partial \mathcal{F}_{k}}{\partial_{\xi}}, \frac{\partial \mathcal{F}_{k}}{\partial_{\eta}}\right]=\left[\boldsymbol{p}_{2}^{k}-\boldsymbol{p}_{1}^{k}, \boldsymbol{p}_{3}^{k}-\boldsymbol{p}_{1}^{k}\right] \tag{106}
\end{equation*}
$$

- With this formula the integration on $T_{k}$ is reduced to integration on $\hat{T}$ and can be evaluated numerically using 2D integration points and weights, $\xi_{p}, \eta_{p}$ and $\omega_{p}$, defined on the reference element $\hat{T}$

$$
\begin{equation*}
\int_{T_{k}} u(x, y) d x d y \approx\left|\operatorname{det}\left(J_{\mathcal{F}_{k}}\right)\right| \sum_{p=1}^{P} \omega_{p} u\left(\mathcal{F}_{k}\left(\xi_{p}, \eta_{p}\right)\right) \tag{107}
\end{equation*}
$$

- Note $\left|\operatorname{det}\left(J_{\mathcal{F}_{k}}\right)\right|$ is two times area of the triangle $T_{k}$.


## 2D and 3D FINITE ELEMENT METHOD

## Evaluation of the Matrix Elements in 2D

- Shape functions on $T$ can be defined using mapping $\mathcal{F}_{k}$ as

$$
\begin{equation*}
N_{i}^{k}:=\hat{N}_{i}\left(\mathcal{F}^{-1}(\boldsymbol{r})\right) \tag{108}
\end{equation*}
$$

i.e.,

$$
\begin{equation*}
N_{i}^{k}(\boldsymbol{r})=\hat{N}_{i}\left(\mathcal{F}_{k}^{-1}(\boldsymbol{r})\right)=\hat{N}_{i}(\hat{\boldsymbol{r}}) \tag{109}
\end{equation*}
$$

where $\mathcal{F}_{k}^{-1}: T_{k} \mapsto \hat{T}$ is the inverse of $\mathcal{F}_{k}, \boldsymbol{r}=(x, y)$ is a point in $T_{k}$ and $\hat{\boldsymbol{r}}=(\xi, \eta)$ a point in $\hat{T}_{k}$.

- Thus, we have

$$
\begin{align*}
\operatorname{alok} 1(i, j) & =\int_{T_{k}} N_{i}^{k}(\boldsymbol{r}) N_{j}^{k}(\boldsymbol{r}) d \boldsymbol{r}=\left|\operatorname{det}\left(J_{\mathcal{F}_{k}}\right)\right| \int_{\hat{T}} \hat{N}_{i}(\hat{\boldsymbol{r}}) \hat{N}_{j}(\hat{\boldsymbol{r}}) d \hat{\boldsymbol{r}},  \tag{110}\\
\operatorname{blok} 1(i) & =\int_{T_{k}} N_{i}^{k}(\boldsymbol{r}) f(\boldsymbol{r}) d \boldsymbol{r}=\left|\operatorname{det}\left(J_{\mathcal{F}_{k}}\right)\right| \int_{\hat{T}} \hat{N}_{i}(\hat{\boldsymbol{r}}) f\left(\mathcal{F}_{k}(\hat{\boldsymbol{r}})\right) d \hat{\boldsymbol{r}} . \tag{111}
\end{align*}
$$

## 2D and 3D FINITE ELEMENT METHOD

## Evaluation of the Matrix Elements in 2D

- The gradients of the nodal shape functions are more complicated.
- Using the chain rule we get (in 2D)

$$
\begin{align*}
& \frac{\partial \hat{N}_{i}(\hat{\boldsymbol{r}})}{\partial \xi}=\frac{\partial N_{i}^{k}(\boldsymbol{r})}{\partial x} \frac{\partial \mathcal{F}_{x}}{\partial \xi}+\frac{\partial N_{i}^{k}(\boldsymbol{r})}{\partial y} \frac{\partial \mathcal{F}_{y}}{\partial \xi},  \tag{112}\\
& \frac{\partial \hat{N}_{i}(\hat{\boldsymbol{r}})}{\partial \eta}=\frac{\partial N_{i}^{k}(\boldsymbol{r})}{\partial x} \frac{\partial \mathcal{F}_{x}}{\partial \eta}+\frac{\partial N_{i}^{k}(\boldsymbol{r})}{\partial y} \frac{\partial \mathcal{F}_{y}}{\partial \eta} . \tag{113}
\end{align*}
$$

- This can be expressed shortly as

$$
\begin{equation*}
\hat{\nabla} \hat{N}_{i}(\hat{\boldsymbol{r}})=J_{\mathcal{F}_{k}}^{T} \nabla N_{i}^{k}(\boldsymbol{r}), \tag{114}
\end{equation*}
$$

where $J_{\mathcal{F}_{k}}^{T}$ is the transpose of the Jacobian matrix of mapping $\mathcal{F}_{k}$.

## 2D and 3D FINITE ELEMENT METHOD

## Evaluation of the Matrix Elements in 2D

- The Jacobian matrix is given as

$$
J_{\mathcal{F}_{k}}(\hat{\boldsymbol{r}})=\left[\begin{array}{ccc}
\frac{\partial F_{x}}{\partial \xi} & , & \frac{\partial F_{x}}{\partial \eta}  \tag{115}\\
\frac{\partial F_{y}}{\partial \xi} & , & \frac{\partial F_{y}}{\partial \eta}
\end{array}\right]=\left[\boldsymbol{p}_{2}^{k}-\boldsymbol{p}_{1}^{k}, \boldsymbol{p}_{3}^{k}-\boldsymbol{p}_{1}^{k}\right] .
$$

- Computing the inverse of $J_{\mathcal{F}_{k}}^{T}$ we get

$$
\begin{equation*}
\nabla N_{i}^{k}(\boldsymbol{r})=\left(J_{\mathcal{F}_{k}}^{T}\right)^{-1} \hat{\nabla} \hat{N}_{i}(\hat{\boldsymbol{r}}) \tag{116}
\end{equation*}
$$

- Matrix elements with gradients of the shape functions are

$$
\begin{align*}
\operatorname{alok} 2(i, j) & =\int_{T_{k}} \nabla N_{i}^{k} \cdot \nabla N_{j}^{k} d \boldsymbol{r} \\
& =\left|\operatorname{det}\left(J_{\mathcal{F}_{k}}\right)\right| \int_{\hat{T}}\left(\left(J_{\mathcal{F}_{k}}^{T}\right)^{-1} \hat{\nabla} \hat{N}_{i} \cdot\left(J_{\mathcal{F}_{k}}^{T}\right)^{-1} \hat{\nabla} \hat{N}_{j}\right) d \hat{\boldsymbol{r}} . \tag{117}
\end{align*}
$$

- 3D is more or less a straightforward extension (3 coordinates, 4 shape functions per tetra, etc.).


## NUMERICAL EXAMPLE

## Capacitance Calculation in Electrostatics

- Maxwell's equations for the static electric field $\boldsymbol{E}$ read

$$
\begin{align*}
\nabla \times \boldsymbol{E}(\boldsymbol{r}) & =0,  \tag{118}\\
\nabla \cdot(\varepsilon(\boldsymbol{r}) \boldsymbol{E}(\boldsymbol{r})) & =\rho_{s}(\boldsymbol{r}), \tag{119}
\end{align*}
$$

where $\rho_{s}$ is the charge density and $\varepsilon$ is the electric permitttivity.

- Since $\nabla \times \nabla u=0$ for an arbitrary sufficiently differentiable function $u$, static electric field $\boldsymbol{E}$ can be expressed using a scalar potential $\phi$

$$
\begin{equation*}
\boldsymbol{E}(\boldsymbol{r})=-\nabla \phi(\boldsymbol{r}) . \tag{120}
\end{equation*}
$$

- Using Maxwell's equation $\nabla \cdot(\varepsilon \boldsymbol{E})=\rho_{s}$ potential $\phi$ satisfies

$$
\begin{equation*}
\nabla \cdot(\varepsilon(\boldsymbol{r}) \nabla \phi(\boldsymbol{r}))=-\rho_{s}(\boldsymbol{r}) . \tag{121}
\end{equation*}
$$

- If $\varepsilon$ is constant, equation (121) reduces to the Laplace equation.

$$
\begin{equation*}
\Delta \phi(\boldsymbol{r})=-\frac{\rho_{s}(\boldsymbol{r})}{\varepsilon} \tag{122}
\end{equation*}
$$

- Thus, in electrostatics we may consider (generalized) Laplace (Poisson) equation for a scalar function.


## NUMERICAL EXAMPLE

## Capacitance Calculation in Electrostatics

Consider a homogeneous PE filled ( $\varepsilon=2.3 \varepsilon_{0}$ ) circular RG-58/U coaxial cable with inner radius $a=0.81 \mathrm{~mm}$ and outer radius $b=2.9 \mathrm{~mm}$.
Assume that the voltage on the inner conductor is +5 V and on the outer conductor the voltage is 0 V . Since the structure is uniform and homogeneous it is sufficient to find the scalar potential on a 2 D cross section of the cable by solving the Dirichlet boundary value problem for Laplace equation

$$
\begin{align*}
2.3 \varepsilon_{0} \nabla^{2} \phi(\boldsymbol{r}) & =0, \quad \boldsymbol{r} \in \Omega  \tag{123}\\
\phi(\boldsymbol{r}) & =5, \quad \boldsymbol{r} \in \Gamma_{a}  \tag{124}\\
\phi(\boldsymbol{r}) & =0, \quad \boldsymbol{r} \in \Gamma_{b} \tag{125}
\end{align*}
$$

Here $\Omega$ is the 2D cross section of the medium between the inner and outer conductors, $\Gamma_{a}$ is the boundary of the inner conductor, $\Gamma_{b}$ is the boundary of the outer conductor, and $\varepsilon_{0}$ is a known constant.

## NUMERICAL EXAMPLE

## Capacitance Calculation in Electrostatics

Find the solution using (2D) FEM and piece-wise linear nodal functions as described before.



Figure: Triangular mesh on the 2D cross section of a coaxial cable (left) and the solution, i.e., the electrostatic potential (right).

## NUMERICAL EXAMPLE

## Capacitance Calculation in Electrostatics

Capacitance $C$ tells how much a structure can store an electrical charge

$$
\begin{equation*}
C=\frac{Q}{U} \tag{126}
\end{equation*}
$$

where $U$ is the potential difference between the conductors, and $Q$ is a net charge. This can be expressed using electrostatic energy $W$ stored in the structure

$$
\begin{equation*}
C=\frac{2}{U^{2}} W \tag{127}
\end{equation*}
$$

where the energy is given by $(\boldsymbol{D}=\varepsilon \boldsymbol{E})$

$$
\begin{equation*}
W=\frac{1}{2} \int_{\Omega} \boldsymbol{E}(\boldsymbol{r}) \cdot \boldsymbol{D}(\boldsymbol{r}) d \boldsymbol{r} . \tag{128}
\end{equation*}
$$

Using electrostatic potential $\phi$, energy can be further written as

$$
\begin{equation*}
W=\frac{1}{2} \int_{\Omega} \varepsilon(\boldsymbol{r}) \nabla \phi(\boldsymbol{r}) \cdot \nabla \phi(\boldsymbol{r}) d \boldsymbol{r} \tag{129}
\end{equation*}
$$

## NUMERICAL EXAMPLE

## Capacitance Calculation in Electrostatics

Thus, capacitance can be expressed as

$$
\begin{equation*}
C=\frac{1}{U^{2}} \int_{\Omega} \varepsilon(\boldsymbol{r}) \nabla \phi(\boldsymbol{r}) \cdot \nabla \phi(\boldsymbol{r}) d \boldsymbol{r} . \tag{130}
\end{equation*}
$$

This can be calculated by using the electrostatic FEM system matrix, i.e., the matrix with elements (without boundary conditions)

$$
\begin{equation*}
A_{m, n}=\int_{\operatorname{spt}\left(u_{m}\right) \cap \operatorname{spt}\left(u_{n}\right)} \varepsilon(\boldsymbol{r}) \nabla u_{m}(\boldsymbol{r}) \cdot \nabla u_{n}(\boldsymbol{r}) d \boldsymbol{r} . \tag{131}
\end{equation*}
$$

On circular domains, both the potential and capacitance have analytical solutions

$$
\begin{align*}
\phi_{\text {ana }}(r) & =\frac{\phi_{b}-\phi_{a}}{\log (b / a)} \log (r / a)+\phi_{a},  \tag{132}\\
C_{\text {ana }} & =2 \pi \varepsilon / \log (b / a) . \tag{133}
\end{align*}
$$

## NUMERICAL EXAMPLE

## Capacitance Calculation in Electrostatics

Compute Relative Root Mean Square (RMS) error of the numerical solution

$$
\begin{equation*}
\frac{\left\|\phi_{\mathrm{num}}-\phi_{\mathrm{ana}}\right\|}{\left\|\phi_{\mathrm{ana}}\right\|}:=\frac{\sqrt{\sum_{m=1}^{M}\left|\phi_{\mathrm{num}}(\boldsymbol{r})-\phi_{\mathrm{ana}}(\boldsymbol{r})\right|^{2} / M}}{\sqrt{\sum_{m=1}^{M}\left|\phi_{\mathrm{ana}}(\boldsymbol{r})\right|^{2} / M}} . \tag{134}
\end{equation*}
$$



Solutions of both $\phi$ and $C$ seem to converge with rate $O\left(h^{2}\right)$. General rule is that FEM approximations of "smooth" functions converge with rate $O\left(h^{2 p}\right)$, where $p$ is the order of the polynomial approximation. Higher order approximations usually give better accuracy with less number of dof, but implementations become (much) more complicated.

## SUMMARY

FEM for finding approximate solutions of boundary value problems arising from partial differential equation-based mathematical modeling of physical phenomena can be summarized as:

1. Develop a BVP for a PDE with information of the domain and boundary.
2. Derive weak formulation of the BVP with appropriate boundary conditions.
3. Generate the mesh, i.e., divide domain $\Omega$ into a finite number of simple elements.
4. Find appropriate conforming and unisolvent discrete FE spaces.
5. Compute the matrix elements and assemble the matrix.
6. Solve the matrix equation.
7. Compute wanted parameters.
